

Briquettes From Sludge in Sewage Treatment Plant: Calorific Power

Stéphanie Rocha^{1,2,a}, Pedro Soares², Lino Maia^{1,3,b*}

¹ CONSTRUCT-LABEST, Faculty of Engineering (FEUP), University of Porto, Rua Dr. Roberto Frias, 4200-465 Porto, Portugal.

² FASA, Santo Agostinho Faculty, Av. Osmane Barbosa, 1179-1199 - Jk, Montes Claros-MG, Brazil.

³ Faculty of Exact Sciences and Engineering, University of Madeira, Campus da Penteada, 9020-105 Funchal, Portugal.

^a up202010607@g.uporto.pt; ORCID: 0000-0002-0984-4897

^b linomaia@fe.up.pt; ORCID: 0000-0002-6371-0179

*Corresponding Author- Lino Maia / linomaia@fe.up.pt

Abstract

Due to the large volume of sewage generated every day, there is a high demand for its treatment. The by-product (called sludge) generated after the treatment process has caused problems in terms of its final disposal. Since the typical end off for this waste is landfills, it is mandatory reducing the landfill amount and the risk of soil contamination. The present work explored an adequate final disposal of the sludge as a sustainable alternative. For this purpose, briquettes were produced using dry sludge from the Sewage Treatment Plant of the Minas Gerais (Brazil) Sanitation Company and vegetable oil used to thicken the briquettes. These briquettes were compared to eucalyptus charcoal in terms of their calorific potential, through immediate analysis, since Brazil has a high demand for primary energy, especially in the industrial sphere. The calorific potential of charcoal reached 16.66 MJ/kg, while that of briquette reached 12.94 MJ/kg. However, briquettes had a density much higher than charcoal, so it takes a smaller volume of briquettes to achieve the same burning capacity as a large volume of charcoal.

Keywords: biomass; briquettes; charcoal; sludge; sustainability.

1. Introduction

With the increase in urbanization in the world, the need to conserve natural resources and the environment has become fundamental for people's quality of life. Thus, the treatment of sanitary sewage is worldwide a problem and it is essential to maintain the quality of water in watercourses (Di Iaconi et al. 2010; Khursheed and Kazmi 2011; Qian et al. 2016; Kacprzak et al. 2017; Lazzari 2018). The sewage generated after the consumption of potable water, whether for residential or industrial use, when released in nature into watercourse, causes significant changes in the aquatic environment, affecting chemical, physical and biological characteristics. The damage caused by sewage to water rivers is due to the large presence of organic matter present in the sewage. Thus, the treatment of wastewater has as its main objective to remove organic matter before it is released into watercourses (Di Iaconi et al. 2010; Carrère et al. 2010; Batista 2015).

A by-product generated from sewage treatment, called sewage sludge, has generated problems regarding its final disposal, since it is produced in large quantities and has toxic characteristics (Jamali et al. 2009; He et al. 2010; Fijalkowski et al. 2017). In Brazil, between 150 and 220 thousand tons of dry matter is produced per year.

38 Currently, the main forms of final disposal of sludge are landfills, incineration, and agricultural use. However,
39 with the large volume generated and the great potential for pollution of sewage sludge, new ways of using the
40 waste have been studied (Okuno et al. 2004; Vieira 2011; Eliche-Quesada et al. 2011; Paris et al. 2016;
41 Geissdoerfer et al. 2017).

42 The expression “sludge” has been used to describe the tailing generated in the sewage treatment process. However,
43 after biological processes, there is a conversion of part of the organic matter that is absorbed, forming sludge, also
44 known as bio-solid, since it is basically composed of biological solids (Andreoli et al. 2001; Lv et al. 2007; Gueri
45 2014).

46 The production and collection of sewage begins in buildings, which can be commercial, residential or industrial,
47 which are the responsibility of the owner. The sewage is conducted to collection systems, which are distinguished
48 by: trunk collector, also known as main collector, receives secondary collectors; the interceptor, which is a network
49 that receives the main collectors and; the emissary, which does not receive any contribution along its route and
50 aims to reach a destination, which may be a lift, final launch or treatment station (COPASA 2022a).

51 The treatment of sanitary sewage has been increasing due to the population growth, the demand for greater service
52 for the population and the investment in new sewage treatment plants (Pedroza 2010; Kacprzak et al. 2017). Thus,
53 even with the emergence of new treatment technologies, the production of sewage sludge will also increase
54 (Andreoli 2006; Kartal et al. 2010; Carrère et al. 2010; Jing et al. 2012; Gu et al. 2017).

55 When the sewage arrives at the treatment plant, sequential procedures are carried out to remove the undesirable
56 substances or make them acceptable for use or final disposal. The treatments have four levels, namely: the
57 preliminary, which is a physical process, which removes coarse solids and sand; the primary, also of a physical
58 nature, removing floating and suspended solids, such as oils, greases and part of the organic matter; the secondary,
59 biological, removing nutrients such as nitrogen and phosphorus, and mainly organic matter and, finally; the
60 tertiary, which can be a complement to the secondary or remove specific substances (COPASA 2022b).

61 The Sanitation Company of Minas Gerais (COPASA) is among the largest sanitation companies in Brazil and is
62 the concessionaire responsible for water supply and sanitary sewage in the city of Montes Claros. Regarding the
63 sewage treatment processes carried out by the company, it is important to know each one of them. Anaerobic
64 Systems is the treatment performed by bacteria that do not require oxygen for respiration, highlighting the Septic
65 Tank, the Anaerobic Filter and the UASB Reactor (Upflow Anaerobic Sludge Blanket). Stabilization Ponds are
66 treatment systems in which the aerobic oxidation or photosynthetic reduction of algae is carried out to stabilize
67 organic matter. Aerobic Reactors with Biofilms, on the other hand, aim to stabilize organic matter by bacteria that
68 develop on a plastic or stone support. It can also be mentioned the disposal in the soil, the surface runoff in the
69 soil, the additive sludge, flotation, ultraviolet and the disposal of the sludge through the generated by-products
70 (COPASA 2022b).

71 In Brazil, the most common way to dispose of sewage sludge is in landfills. There are two ways to dispose of this
72 waste in landfills: (i) the first is to manage the sewage sludge together with the collection of urban solid waste,
73 and (ii) the second is the construction of a sanitary landfill for the sludge. In most cases, the sludge is disposed of
74 together with urban solid waste (Vieira 2011).

75 Landfills are considered the cheapest method to dispose of sewage sludge. However, it can cause several problems,

76 such as: leaching, groundwater pollution, soil contamination and methane gas emissions. In addition to the
77 environmental risks involved in disposing of sewage sludge in landfills, it is difficult to find areas to receive new
78 landfills. There is a concern with the useful life of active landfills, since sewage sludge demands a large volume
79 for its management (Silvério 2004; Qian et al. 2016; Kacprzak et al. 2017; Gherghel et al. 2019).

80 In some sewage treatment plants the incineration process is adopted, wherein the thermal destruction of the waste
81 takes place by exposing the sludge to temperatures higher than 1000 °C. The result of this process is an ash, with
82 reduced volume in relation to sewage sludge. This ash must be disposed of in appropriate landfills and the gases
83 that must be treated, for instance, being used as a source of energy (Massanet-Nicolau et al. 2010; Kargbo 2010;
84 Vieira 2011; Cao and Pawłowski 2012; Pastore et al. 2013; Gong et al. 2014; Cano et al. 2015; Gianico et al. 2015;
85 Carlsson et al. 2016).

86 In the incineration process, the mass of sewage sludge is reduced by up to 5 times, leaving only fixed solids, called
87 ash. This alternative is used when there are no areas available to handle the waste in landfills or the sludge
88 contamination is very high. However, sludge incineration requires a large amount of energy and is potentially
89 polluting for the atmosphere, therefore, a high investment in filters to retain the toxic gases produced is needed
90 (Andreoli et al. 2001). One of the ways to equate the high investment to incinerate sewage sludge is the possibility
91 of reusing the calorific potential of the sludge generated in the sewage treatment plant (Vieira 2011).

92 Among the conventional alternatives for the final disposal of sewage sludge, the most economically and
93 environmentally viable is agricultural use, since the sludge is rich in nutrients and organic matter (Andreoli 2006).
94 Besides being an important source of organic matter, when applied to the soil, the sludge provides an increase in
95 productivity, a decrease in the use of fertilizers, increases soil resistance and increases its water retention capacity
96 (Vieira 2011).

97 However, the presence of heavy metals and pathogenic organisms can make the use of sewage sludge in agriculture
98 unfeasible (Jamali et al. 2009; He et al. 2010; Vieira 2011; Fijalkowski et al. 2017). Depending on the origin of
99 the sewage, the type of treatment and efficiency, the presence of heavy metals and pathogenic organisms can vary
100 from low or non-existent to very high, so it is necessary to evaluate all these aspects for the use of sludge in
101 agriculture (Andreoli et al. 2001).

102 Due to the high-risk potential shown by the contaminants that can be identified in sewage sludge, the Brazilian
103 National Council for the Environment (CONAMA) has drawn up a resolution governing the use of sewage sludge
104 as fertilizer (Vieira 2011). The Brazilian Resolution No. 375, of August 29, 2006, “defines criteria and procedures
105 for the agricultural use of sewage sludge generated in sanitary sewage treatment stations and its by-products
106 (ABNT)”. The resolution brings aspects related to the quality parameters of the sewage sludge, the characteristics
107 of the application sites, among others.

108 In addition, another important point to ensure the well-being of the population, availability of natural resources
109 with the quality and quantity needed for future generations, it is necessary to create new renewable energy sources
110 (Di Maria et al. 2016; Geissdoerfer et al. 2017; Gherghel et al. 2019). Since, Brazil has a great challenge about
111 energy issues. During the 20th century there was an intense economic development in Brazil, which was reflected
112 in a greater demand for primary energy, that is, energy from renewable sources (Tolmasquim et al. 2007).

113 Due to the large volume of sludge produced daily and considering population growth, the traditional way of

114 disposing of this waste will become unfeasible, both environmentally and economically (Kelessidis and Stasinakis
115 2012). In addition, the large-scale production of industries that demand thermal energy coming mainly from the
116 burning of charcoal causes an increase in illegal deforestation of Brazilian forests. Thus, producing energy with
117 residual biomass from effluent treatment plants is a viable alternative, since there is a large supply of this residue
118 worldwide (Kargbo 2010; Cao and Pawłowski 2012; Manara and Zabaniotou 2012; Pastore et al. 2013; Gong et
119 al. 2014; Cano et al. 2015; Carlsson et al. 2016; Lazzari 2018).

120 The use of sludge as an alternative energy at low cost is verified in a study carried out with distillery sludge, in
121 which different combinations between sludge and coal were proposed, in the proportions of 25%, 40%, 50% and
122 75% by weight. The best combination found was 40% sludge with 60% charcoal, with a calorific potential of 4659
123 kcal/kg (Dhote et al. 2020). Therefore, in addition to promoting low-cost energy, it also reduces the release of this
124 effluent into the environment.

125 Others recent studies have also evaluated the calorific potential of materials such as chestnut shells (Jiang et al.
126 2018), residual vegetable oil (Dey et al. 2021) and empty bunches of palm oil (Yan et al. 2019). As the chestnut
127 shells have cellulose, hemicellulose and lignin with low calorific value, a methodology to produce a biochar by
128 catalytic pre-oxidation and pyrolysis with sulfuric acid and urea was proposed. The changes in the structure
129 promoted the production of a high-quality coal with high calorific value (Jiang et al. 2018).

130 An optimized model that contained a mixture of fuel with residual vegetable oil was compared with diesel. The
131 results showed this mixture has a calorific value and density comparable to diesel, in addition to a cleaner emission
132 during engine operation (Dey et al. 2021).

133 Therefore, the objective of this study is to explore and contribute for an adequate destination for the sludge as a
134 sustainable alternative, producing and analyzing briquettes, having as raw material the sludge from the sewage
135 treatment plant, to be used as heat sources, totally or partially replacing vegetable coal. At the end of this work, it
136 was hoped to find a viable alternative to dispose of sewage sludge, in addition to increasing the useful life of
137 sanitary landfills, reducing the risk of soil contamination and the use of charcoal in the industrial scope.

138 **2. Material and methods**

139 For the present work, the sludge specimens were collected, as described in the Brazilian standard NBR 10007 –
140 Sampling of solid waste (ABNT 2004), in the sewage treatment station of the Sanitation Company of Minas Gerais
141 (COPASA) which handles all sewage generated in the city of Montes Claros. For the charcoal specimens,
142 eucalyptus charcoal was used. After the production of sewage sludge briquettes and purchase of charcoal, the
143 calorific value of the specimens was calculated, and its bulk density was determined.

144 **2.1. Briquette production**

145 The dry sewage sludge specimens were collected after the thermal drying process (Fig. 1), therefore, the
146 specimens were homogeneous.

147



148

149

Fig. 1. Collection of specimens in the thermal dryer.

150 Sewage Treatment Station, in Montes Claros, Minas Gerais, performs the dehydration and desiccation of the sludge
151 through thermal drying. The equipment used is a rotating drum that performs mixed drying, which is a combination
152 of direct drying, called convection, and indirect drying, known as conduction (LOBATO 2011).

153 Direct drying involves the passage of hot air over the sludge (SANIN et al. 2010). The advantage of its use is
154 greater heat exchange, as there is direct contact between the drying medium and the sludge (DAVID 2002). In this
155 study, the rotary dryer has an inclined rotating cylindrical shell, which causes the sludge and drying medium to
156 move to the end of the drum, while the rotation mixes them.

157 In indirect drying, the dryers do not come into contact with the sludge, causing heat transfer by conduction
158 (DAVID 2002). The main advantage is the low production of dust and almost no air pollution, but it has a lower
159 drying efficiency when compared to direct drying, recommending the use of a combination of both (SANIN et al.
160 2010).

161 The liquid sludge is discharged from the Upflow Anaerobic Reactors (UAR), containing a solids content of 3%
162 and dehydrated in a centrifuge, concentrating approximately 25% of solids. After that, it is sent to the thermal
163 dryer, with temperatures of 350°C in a period of 30 minutes, transforming it into a sterilized granular material
164 (COMPANHIA DE SANEAMENTO DE MINAS GERAIS (COPASA) 2011). Briquettes with different
165 proportions of residue/binder were prepared, as shown in Fig. 2, in order to find the best agglutination composition
166 for the briquettes. Wasted vegetable oil was used as a binder.

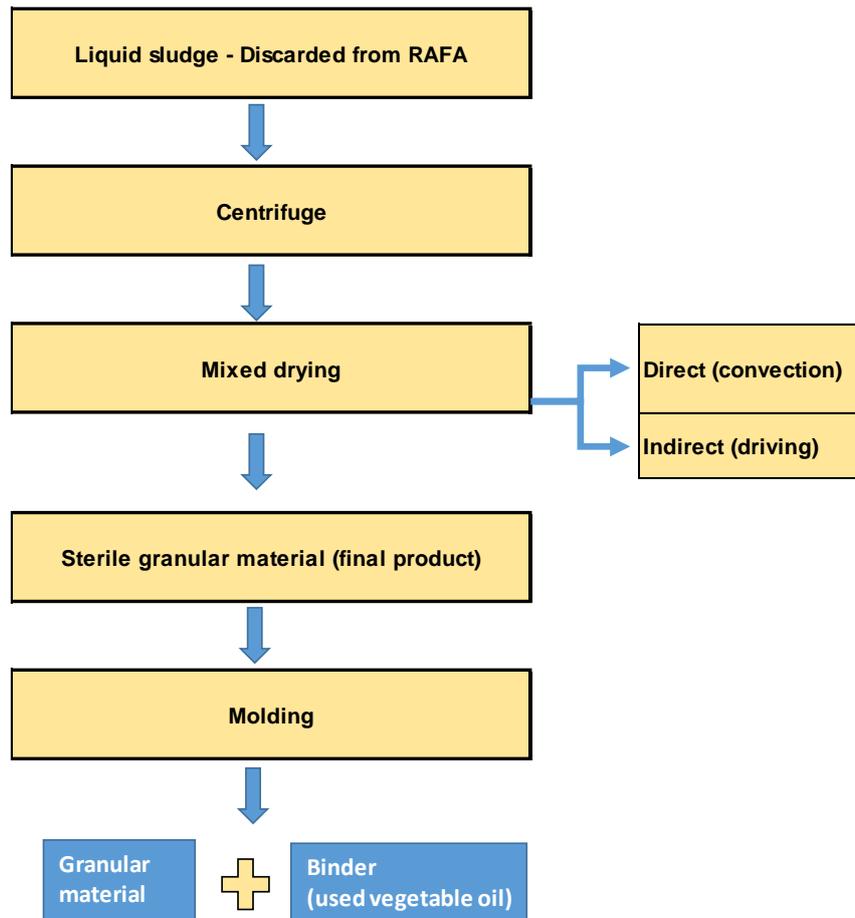


167

168

Fig. 2. On the left, the briquettes on the molding day, and on the right, after drying.

169 For each individual briquette, 200 g of dry sludge and 30 ml of vegetable oil were mixed. The specimens were
170 placed in cylindrical molds with 100 mm of diameter and 50 mm height and pressed with a compaction hammer,
171 thus the final height being approximately 25 mm. Then, they were unmolded with a specimen extractor and
172 exposed to laboratory conditions for 48 hours (wherein the temperature was about 25 °C and the relative humidity
173 about 60%). Fig. 3 shows the sequence of processes used to obtain sludge briquettes:



174

175

Fig. 3. Sequence of processes used to obtain sludge briquettes.

176 **2.2. Immediate analysis**

177 The sludge analysis was carried out according to the Brazilian standards: NBR 8112 – Charcoal: Immediate
 178 analysis (ABNT 1986), SANS 5924 - Moisture content of coal specimens intended for general analysis (Standard
 179 2009) and ISO 562 – Hard coal and coke - Determination of volatile matter (International organization for
 180 standardization 2010), which applies to the determination of moisture content, ash, volatile materials, and fixed
 181 carbon.

182 To determine the calorific value, the equation developed in Ref. (Parikh et al. 2005) was used, which correlates
 183 the fixed carbon content, the content of volatile materials and the ash content to determine the calorific value in
 184 MJ/kg with absolute error of 3.74%.

185 **2.3. Moisture content**

186 According to the Brazilian standards NBR 8112 (ABNT 1986) and SANS 5924 (Standard 2009), the determination
 187 of the moisture content was done as follows: between 1 to 2 g of the sludge briquette specimen was collected with
 188 the aid of a balance. Then, the sample was taken to an oven previously heated to 105 °C where it remained for 90
 189 minutes. At the end of the process, the specimens were taken to the desiccator to cool and avoid humidity. After
 190 cooling, the final mass was determined. Thus, the moisture content could be determined from Equation 1.

191
$$\%H = \frac{m_1 - m_2}{m_1} \times 100 \quad (1)$$

192 Where:

193 %H is the moisture content, in percentage;

194 m1 is the initial mass of the sample, in grams;

195 m2 is the final mass of the sample, in grams.

196 According to the standard, three specimens of each material were analyzed to determine the moisture content.

197 **2.4. Volatile material content**

198 According to NBR 8112 (ABNT 1986) and ISO 562 (International organization for standardization 2010), the
 199 percentage of volatile material was determined from previously dried briquette specimens. A dry specimen with
 200 ~1 g was taken to a muffle with a maximum temperature of 950 °C following the steps (Table 1):

201 Table 1. Step-by-step determination of volatile material content (Source: ISO 562, 2010)

Procedure	Time	Temperature (°C)
Crucible at the door	Two minutes	300
Crucible inside the muffle with the door open	Three minutes	500
Crucible inside the muffle with the door closed	Six minutes	950

202

203 Therefore, the percentage of volatile material could be determined from Equation 2.

204
$$VM = \frac{m_2 - m_3}{m_2} \times 100 \quad (2)$$

205 Where:

206 VM is the percentage of volatile materials;

207 m2 is the mass of the dry sample before place in the muffle, in grams;

208 m3 is the mass of the dry sample after cooling, in grams.

209 According to the standard, three samples of each material were analyzed for the determination of volatile materials.

210 **2.5. Ash content**

211 According to NBR 8112 (ABNT 1986), the determination of the ash content was found by following the steps: ~1
 212 g of a dry specimens was placed in a crucible. The set was placed in a muffle previously heated to 700 °C and
 213 remained for one hour. After this process, the specimen was taken to the desiccator to cool and avoid humidity.
 214 After cooling, the final mass of the set was determined.

215 Thus, the determination of ash content could be determined from Equation 3.

216
$$AC = \frac{m_1 - m_0}{m} \times 100 \quad (3)$$

217 Where:

218 AC is the ash content, in percentage;
219 m1 is the mass of the set crucible with sample ash after cooling, in grams;
220 m0 is the mass of the crucible, in grams;
221 m is the initial dry mass of the sample before place in the muffle, in grams.
222 According to the standard, three specimens of each material were analyzed to determine the ash content.

223 **2.6. Fixed carbon content**

224 According to NBR 8112 (ABNT 1986) the fixed carbon content was obtained through the difference of Equation
225 4.

$$226 \qquad \qquad \qquad FC = 100 - (AC + VM) \qquad \qquad \qquad (4)$$

227 Where:

228 FC is the fixed carbon content, in percentage;
229 AC is the ash content, in percentage;
230 VM is the volatile materials, in percentage.

231 **2.7. Determination of calorific power**

232 The determination of the calorific value was carried out from the correlation of the immediate analysis developed
233 (Parikh et al. 2005).

$$234 \qquad \qquad \qquad CP = (0.3536 * FC) + (0.1559 * VM) + (0.0078 * AC) \qquad \qquad \qquad (5)$$

235 Where:

236 CP is the calorific power, in megajoule per kilogram;
237 FC is fixed carbon content, in percentage;
238 AC is the ash content, in percentage;
239 VM is the percentage of volatile materials.

240 **2.8. Apparent density**

241 To calculate the bulk density, a balance was used to define the briquette mass. The briquette volume was calculated
242 based on its dimensions with the aid of a caliper. With that, Equation 6 is used to define the bulk density:

$$243 \qquad \qquad \qquad D = \frac{m}{v} \qquad \qquad \qquad (6)$$

244 Where:

245 D is the bulk density, in kilograms per cubic meter;
246 m is the mass of the briquette, in kilograms;

247 v is the external volume of the briquette, in cubic meters.

248 3. Discussion

249 After molding and visual analyze the briquettes with varying proportions of residue/adhesive, the best consistency
250 was achieved when 200 g dry sludge were mixed with 30 ml of waste vegetable oil. Table 2 shows the results of
251 the immediate analysis applied to the specimens of sludge and charcoal briquettes. The average of the results
252 obtained in the tests in three specimens was considered.

253 Table 2. Comparison of immediate analysis on specimens.

Specimens	Moisture (%)		Volatile Materials (%)		Ash content (%)		Fixed Carbon** (%)
	M _i	Average	VM _i	Average	AC _i	Average	Average
(A) Sludge Briquettes	3.0		57.5		38.3		
	3.5	3.5	47.8	49.3	31.5	36.6	14.0
	3.9		42.8		40.1		
(B) Charcoal	2.0		63.1		20.2		
	3.4	2.4	62.6	60.2	-16.8*	19.6	20.1
	1.8		54.9		19.0		

254 * This value was considered an outlier, probably there was an error during recording the initial mass.

255 ** Fixed Carbon was determined using the average values of the volatile materials and the ash content.

256 As shown in Table 2, the sludge briquette specimens had higher moisture and ash content but lower volatile
257 materials and fixed carbon content than the charcoal. The excess moisture in the biomass reduces the burning
258 capacity, as the calorific value decreases, thus increasing the consumption of matter (Vieira 2011). The fixed
259 carbon content has a direct influence on the calorific value, as the higher the fixed carbon, the greater the material's
260 burning potential (Filho 2013).

261 Ash is the inorganic material remaining after burning a fuel (Filho 2013). The high concentration of ash reduces
262 the calorific power of the material, since the ash does not participate in combustion (Vieira 2012). After testing
263 the ash content, it was possible to identify that charcoal loses approximately 80% of its mass after burning and that
264 briquettes lose 63%, leaving a considerable volume of inorganic material after burning (Fig. 4).



265

266 Fig. 4. On the left, ashes derived from burning specimens of coal. On the right, ashes obtained burning sludge
 267 derived briquettes.

268 Volatile materials are the fraction that vaporizes when the material is heated under certain conditions. Table 3
 269 presents the results of the calorific value and density of the specimens.

270

Table 3. Comparison of calorific value and bulk density.

Sample	Calorific Value (MJ/kg)	Apparent Density (kg/m ³)
(A) Sludge Briquettes	12.9	1157.3
(B) Charcoal	16.7	190.0

271

272 To assess the energy potential of a combustible material, the most important property is the calorific power (Filho
 273 2013). Specimens of charcoal and sludge briquettes showed distinct values of calorific power, with the charcoal
 274 being 29% greater than that of sludge briquettes. However, the apparent density of specimens from sludge
 275 briquettes (when tightly packed) is about six times greater than that of the charcoal. Therefore, in terms of volume
 276 storage, sludge briquettes have an advantage when compared with the charcoal.

277 The calorific value of vegetable oil according to national manufacturers is 34.13 MJ/l (8,125 kcal/l). The density
 278 of a refined vegetable oil is 0.918 g/ml, whereas for used oil it is 0.908 g/mL (FROEHNER, S.; LEIRHOLD, J.;
 279 LIMA JÚNIOR 2007). Therefore, considering that each sludge briquette was composed by 30 ml (~27.2 g) of
 280 used vegetable oil and 200.0 g was sludge (i.e. the mass of the used vegetable oil was 12.0% of total the mass of
 281 the briquette) the calorific capacity of a used vegetable oil contributes with almost 35% of the total calorific
 282 capacity of the sludge briquette. Consequently, the calorific value of sewage sludge is estimated in 9.58 MJ/kg.
 283 This value agrees with the ones found in Durdević et al. (2019), but they are lower than the ones reported in
 284 Ostojski (2018) or in Gueri (2014) – wherein it was reported 17.89 MJ/kg for the sludge with 20% moisture.

285 It is worth mentioning that vegetable oil is widely used in Brazil and around the world. However, its incorrect
 286 disposal causes a lower availability of this material for reuse as fuel and as a binder, which is what is proposed in
 287 this discussion. The Conama Resolution n°. 362/2005 (CONAMA 2005) prohibits any disposal of used or
 288 contaminated oils in soils, subsoils, inland waters. It is important to create adequate policies that favor the efficient
 289 collection and disposal of this material.

290 From the legislative aspect in Brazil, the regulation for the emission of pollutants is the CONAMA 436/2011

291 (CONAMA 2011) which establishes the emission limits of waste by type of pollutant and type of source, according
292 to its annexes present. The environmental inspection and licensing agency must consider the local conditions of
293 the polluting source and its area of influence, determining emission limits and air quality management, if necessary.
294 There is no current resolution for briquettes with sewage sludge, however, Annex III and Annex IV present in this
295 resolution can serve as a reference, since they are biomass. The Annex III establishes emission limits for air
296 pollutants from heat generation processes from the combustion of sugarcane biomass and Annex IV deals with
297 emission limits for air pollutants from heat generation processes at from the external combustion of wood
298 derivatives. These annexes establish the regulated pollutants, the rated power ranges, and the emission limit
299 concentration of particulate matter.

300 **4. Conclusions**

301 Through the analysis and determination of the calorific potential of the sewage sludge and charcoal briquettes, it
302 is concluded that the briquettes, manufactured with dry sewage sludge and used vegetable oil, have a calorific
303 power lower than the charcoal. However, since the sewage sludge briquettes have much higher apparent density
304 that the charcoal, the calorific potential per volume unit is bigger for the sewage sludge briquettes.

305 As a large amount of sewage sludge is produced daily, the use of briquettes of sewage sludge with used vegetable
306 oil looks to be a viable alternative to replace charcoal as a heat source in the industrial sphere, especially where
307 low or medium temperatures are required. The use of sludge briquettes as renewable energy is an option among
308 the types of biomass fuel production. Adopting this end of for sewage sludge, it is provided an increase in the
309 useful life of landfills and reduce soil contamination because this material has a high potential for contamination
310 and occupies a large volume that would be removed from the landfills. In addition, the replacement of charcoal by
311 sewage sludge briquettes with used vegetable oil will reduce the deforestation of wood for charcoal production
312 and will bring a renewable energy alternative with a high potential.

313 It is suggested for future studies the quantification of pollutants generated during the combustion process, the
314 application of new materials as a binder, in addition to economic availability.

315

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329 Stéphanie Rocha – Data curation, Funding acquisition, Methodology, Resources, Writing – original draft,
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331 Pedro Soares – Formal analysis, Investigation, Writing – original draft

332 Lino Maia – Conceptualization, Funding acquisition, Supervision, Validation, Writing – review & editing

333 **Competing Interests**

334 The authors declare that they have no competing interests

335 **Availability of data and materials**

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