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5	Are TiO <sub>2</sub> -based exterior paints useful catalysts for gas-phase			
6	photooxidation processes? A case study on <i>n</i> -decane abatement for air			
7	detoxification			
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#### 26 Abstract

27 *n*-Decane is a saturated long-chain hydrocarbon, belonging to the family of the 28 volatile organic compounds (VOCs), which is persistently present in indoor air of several 29 industrial closed facilities. Due to the VOCs environmental impact, all efforts that have 30 been made during the last decades to degrade this kind of air pollutants are extremely 31 important. Accordingly, the present paper reports *n*-decane photooxidation studies carried 32 out in an annular photoreactor under simulated solar irradiation and employing a catalytic 33 bed made of cellulose acetate monoliths coated with a photocatalytic paint. The influence 34 of the feed flow rate, *n*-decane concentration, relative humidity, and incident irradiance 35 on the *n*-decane degradation kinetics was assessed. Within this work, *n*-decane 36 photodegradations higher than 90% were achieved, depending on the experimental 37 conditions. Additionally, a phenomenological reaction rate model of the *n*-decane 38 photocatalytic oxidation was proposed and assessed. The proposed model assumes that 39 *n*-decane and water molecules compete for different active sites on the catalyst surface. 40 Finally, despite the high *n*-decane photodegradation achieved, reaction by-products were 41 identified and, based on these compounds, a reaction mechanism was formulated.

42

Keywords: Photocatalysis; Air Decontamination; *n*-Decane; Photo-TiO<sub>2</sub> Paint; Acetate
Cellulose Monoliths; Artificial Sunlight.

#### 45 **1. Introduction**

46 For a long time, society has been debating indoor air pollution and its effect on 47 human health whether in urban or industrial areas [1-4]. Today, 70-90% of our lifetime is spent at indoor environments [5, 6]. Incoming air filters or air cleaners based on 48 49 ultraviolet germicidal irradiation, activated carbon, ionization, or ozone generation are 50 the most used methods for air decontamination [3, 7]. Nevertheless, photocatalysis is now 51 seen as a valuable option for de-polluting purposes [8-15], mainly because it: i) can be 52 operated at room temperature [16]; ii) air (through water vapour and molecular oxygen) 53 can be used as the source of oxidant [17], iii) degrades/mineralizes a wide range of 54 organic pollutants into harmless or easily neutralized final products (CO<sub>2</sub>, H<sub>2</sub>O and 55 mineral acids) [18]; iv) can take advantage of solar radiation for performing the charge 56 separation at the semiconductor [19]. Furthermore, semiconductor titanium dioxide 57 (TiO<sub>2</sub>) is commonly employed as photocatalyst in photocatalytic oxidation (PCO) processes due to its inexpensiveness, resistance to photocorrosion, high oxidative power, 58 59 and relatively low toxicity [20-22].

As reported in our previous work [23], high concentrations of *n*-decane (up to 300 μg m<sup>-3</sup>) were found in the indoor air of a WWTP with closed facilities at different sampling sites and campaigns; thus, *n*-decane was used as organic air pollutant model.
The solar PCO of *n*-decane over TiO<sub>2</sub> for air detoxification can be represented by eq. 1 [10]:

65 
$$C_{10}H_{22}(g) + \frac{31}{2}O_2(g) \xrightarrow{\text{TiO}_2, h\nu} \text{intermediates} \xrightarrow{\text{TiO}_2, h\nu} 10 \text{ CO}_2(g) + 11 \text{ H}_2O(g) \quad (eq. 1)$$

and considering what is believed to be the initial stages of the photocatalytic process, thefollowing equations are the most representative [24-27]:

68 
$$\operatorname{TiO}_2 + h\upsilon \longrightarrow e_{cb}^-(\operatorname{TiO}_2) + h_{vb}^+(\operatorname{TiO}_2)$$
 (eq. 2)

69 
$$h_{vb}^+(TiO_2) + H_2O \longrightarrow HO^{\bullet} + H^+$$
 (eq. 3)

70 
$$h_{vb}^+(TiO_2) + HO^- \longrightarrow HO^-$$
 (eq. 4)

71 
$$e_{cb}^{-}(TiO_2) + O_2 \longrightarrow O_2^{\bullet-}$$
 (eq. 5)

72 
$$HO^{\bullet} + RH \longrightarrow RH^{\bullet+} \longrightarrow R^{\bullet} + H^{+}$$
 (eq. 6)

73 
$$h_{vb}^+(TiO_2) + RH \longrightarrow RH^{\bullet+} \longrightarrow R^{\bullet} + H^+$$
 (eq. 7)

74 
$$O_2^{\bullet-} + H^+ \longrightarrow HOO^{\bullet}$$
 (eq. 8)

75 
$$O_2^{\bullet-} + HOO^{\bullet} + H^+ \longrightarrow H_2O_2 + O_2$$
 (eq. 9)

Conduction-band electrons  $e_{cb}^{-}(TiO_2)$  and valence-band holes  $h_{vb}^{+}(TiO_2)$ , i.e. 76 electron-hole pairs, are generated when photons of energy  $h\nu$  matching or exceeding the 77 78 semiconductor band-gap energy are absorbed (eq. 2). Once at the surface of the semiconductor, and on the absence of any suitable acceptor (for  $e_{cb}^-$ ) and donor (for  $h_{vb}^+$ ) 79 80 recombination will occur in a matter of nanoseconds; therefore no reaction occurs [16, 81 27]. Hydroxyl anions and water molecules adsorbed on TiO<sub>2</sub> surface, act as electron 82 donors, while molecular oxygen acts as electron acceptor, leading to the formation of 83 hydroxyl (HO<sup>•</sup>) and superoxide ( $O_2^{\bullet-}$ ) radicals [24-26] (see eq. 3-5). When an organic 84 molecule (RH) is adsorbed onto semiconductor surface, the reaction with hydroxyl radical 85 occur, followed by structural breakdown into several intermediates until, eventually, total 86 mineralization (see eq. 6) [10, 28]. The photogenerated holes due to the high oxidation 87 potential can also participate in the direct oxidation of the organic pollutants (eq. 7) [29, 30]. Peroxide (HOO<sup>•</sup>) radical can also be generated from the protonation of  $O_2^{\bullet-}$  radical 88 89 and subsequently form hydrogen peroxide (see eq. 8-9).

TiO<sub>2</sub> powders have been incorporated as white pigment in different applications from ancient times [31]. As early as 1929, Kiedel [32] stated that titanium white pigment, under sunlight irradiation, was responsible for paint chalking because the photodegradation of organic binder. In 1938, Goodeve *et al.* [33] reported that UV absorption produces active oxygen species on the TiO<sub>2</sub> surface that cause dyes tophotobleach.

96 Although, it was during the 1960s that, for the first time, TiO<sub>2</sub> photochemical 97 effect was used to induce chemical reactions [34, 35], Mashio and coworkers [36] in 1956 98 conducted several studies regarding oxidation induced by TiO<sub>2</sub> under illumination. These 99 works concluded that anatase is more photoactive than rutile. However, the first 100 contribution for understanding the heterogeneous photocatalytic effect was in 1972 with 101 the pioneer work by Fujishima and Honda [37]. These authors investigated the 102 electrochemical photolysis of water using a single TiO<sub>2</sub>-rutile crystal (n-type) as 103 photoanode and a Pt counter electrode. This work opened the frontiers for the use of 104 titania for photocatalysis and other applications.

105 Construction materials can be used to support photocatalytic TiO<sub>2</sub> nanoparticles 106 and used as depolluting agents [31, 38-44]. Paint coatings, among all construction 107 materials, are especially attractive as support for photocatalytic TiO<sub>2</sub> since almost all 108 surfaces in urban areas can be painted. Bygott et al. [38], for instance, report a field trial 109 in London, close to a school children playground, where an area of 300  $m^2$  of walls was 110 painted with a silicate-based paint incorporating 7.5 wt.% of photocatalytic TiO<sub>2</sub>. The results showed a daily NO<sub>x</sub> abatement of ca. 4.5 g in about 10 000  $\text{m}^3$  of air around the 111 112 school children playground [38]. Maggos *et al.* [44] report NO<sub>x</sub> depollution tests in an 113 artificially closed parking area, which was polluted by a car exhaust during the testing 114 period; they observed a reduction of 19 % and 20 % for NO and NO<sub>2</sub>, respectively. 115 Salthammer and Fuhrmannh [43] studied the photocatalytic efficiency of two different types of commercially available wall paints in a 1 m<sup>3</sup> test chamber with and without air 116 exchange using artificial daylight. The results showed that formaldehyde was 117

photooxidise under static conditions. In contrast, for typical VOCs, under dynamicconditions, no significant photocatalytic effect was observed.

120 Several studies indicate that paint components can impair the photoactivity of paint films [42-50]. For example, Allen et al. [46] studied the effect of different paint 121 122 components on the photoactivity of these paints. The results showed that the porosity, 123 which is related to the particulated paint components (pigments and extenders) 124 concentration, has a positive effect on photoactivity. However, higher content in CaCO<sub>3</sub> 125 and high porosity makes paints prone to self-degradation. In the same line, Mendes and 126 co-workers [41, 51, 52] developed a vinyl exterior paint modified with several TiO<sub>2</sub> 127 photocatalysts: P25 (Evonik/Degussa), PC50 (Millennium), PC105 (Millennium), PC500 128 (Millennium), ANX type PA (Kemira), UV100 (Sachtleben), AMT100 (Tayca), 129 UVLP7500 (Kronos), VLP7000 (Kronos), and VLP7101 (Kronos); the authors stated that 130 paint pigmentary TiO<sub>2</sub> is the most critical component affecting the photocatalytic activity 131 for NO<sub>x</sub> abatement due to its competitive absorption of the UV radiation. Considering the 132 results reported by these authors, the highest yields towards NO<sub>x</sub> photocatalytic oxidation 133 are obtained when incorporating in paint formulations photocatalysts PC500 134 (Millennium), PC105 (Millennium), and UV100 (Sachtleben) [41, 51, 52]

135 Although the potential of photocatalytic paints to detoxify air is very promising, 136 several studies demonstrate the formation of by-products that may be harmful for humans 137 [45, 53-55]. For example, Uhde and Salthammer [54] reported that UV-irradiated paints 138 produce undesired and highly toxic by-products such as formaldehyde, acetaldehyde, 139 ethylacrolein, pentanal, 1-hydroxy-butanone, and hexanal. This observation was further 140 emphasized by Kolarik and Toftum [53]. Auvinen et al. [45] and Geiss et al. [55] found 141 that relatively high amounts of organic compounds, such as aldehydes and ketones, are 142 formed from the decomposition of binders and additives. Auvinen et al. [45] also stated 143 that photocatalytic surface aging and the use of different substrates (glass, gypsum or 144 polymeric plaster) do not have a noteworthy influence on the paint photocatalytic activity. 145 Disinfection of air using photocatalytic paints was the focus of other research 146 groups [47, 50, 56]. According to Hochmannova and Vytrasova [47], UV light emitted 147 from normal domestic fluorescent lights is capable to ensure the photocatalytic and 148 antimicrobial effects of paints incorporating nanoparticles of zinc oxide. Later, Sousa et 149 al. [50] showed microorganism photoinactivation over a photocatalytic paint under UVA 150 irradiation.

151 Although photocatalytic paints have been showing very promising results 152 concerning the photodegradation of air pollutants and the photoinactivation of 153 microorganisms, it is necessary to keep improving their performance paints as well as 154 understand the phenomena behind their photoactivity. This paper presents a study on gas-155 phase solar photooxidation of *n*-decane over a TiO<sub>2</sub>-containing paint, using a lab-scale 156 continuous-flow annular photoreactor with a compound parabolic collector. To the best 157 of our knowledge, this is the first time that the performance of TiO<sub>2</sub>-based exterior paints 158 and their applicability on gas-phase photooxidation processes for *n*-decane abatement is 159 evaluated. The photocatalytic oxidation of n-decane was studied for different operating 160 conditions, such as feed flow rate, n-decane concentration, feed relative humidity and 161 incident irradiance. The *n*-decane degradation reaction behaviour in the continuous 162 system was modelled considering different Langmuir-Hinshelwood kinetic-based 163 reaction rate equations. It considers that PCO of *n*-decane is not influenced by reaction 164 intermediates and/or products and *n*-decane and water are the major species. In addition, 165 a reaction mechanism was proposed for *n*-decane PCO considering the degradation by-166 products identified by GC/MSD.

#### 167 **2. Experimental**

#### 168 2.1. Materials and chemicals

169 Mendes and co-workers [41, 51, 52] reported a water-based vinyl paint loaded 170 with TiO<sub>2</sub> photocatalyst PC500 (Millennium) that produced high NO conversions among 171 several other commercially available photocatalysts. For this reason the same modified 172 vinyl paint with photo-TiO<sub>2</sub> PC500 was selected. The PC500 photocatalyst properties are 173 detailed in Table 1. Cellulose acetate monoliths (named C: TIMax CA50-9/S - $L_{\rm C} = 80$  mm,  $d_{\rm ch}^2 = 9$  mm × 9 mm,  $e_{\rm w,ch} = 0.1$  mm; Wacotech GmbH & Co. KG.) were 174 175 used to support the catalytic paint. For the generation of humidified air streams 176 contaminated with *n*-decane, deionized water and *n*-decane ( $\geq$  94%; CAS no. 124-18-5; 177 Merck) were used without further purification. Air Liquide provided all gases, with 178 minimum total purities of 99.999%: helium N50, nitrogen N50, and synthetic air N50 179  $(O_2: 20 \pm 1\%; H_2O: < 3 \text{ ppm}; C_nH_m: < 0.1 \text{ ppm}; CO_2: < 1 \text{ ppm}; CO: < 1 \text{ ppm}).$ 

#### 180 2.2. Photocatalytic films preparation and characterization

181 Photo-TiO<sub>2</sub> PC500 from Millennium) was used to modify a commercially 182 available exterior water-based vinyl paint. The catalyst and paint properties are 183 summarized in Table 1 [52]. From the original exterior water-based vinyl paint, half of 184 the pigmentary TiO<sub>2</sub> (9 wt.% in wet base) was removed; the photocatalytic paint 185 (henceforth named as P) was, subsequently, formulated by adding 9 wt.% of photo-TiO<sub>2</sub> 186 PC500 (ca. 50 cm<sup>3</sup> of paint without 50% of pigmentary TiO<sub>2</sub> and mixing for 30 min at 187 300 rpm in a 100 cm<sup>3</sup> stainless steel vessel), as reported by Águia *et al.* [41]. The final 188 photo-TiO<sub>2</sub> PC500 and pigmentary TiO<sub>2</sub> content was 9 wt.% in wet basis (ca. 17 wt.% in 189 dry basis) (see Table 1).

190 Cellulose acetate monoliths were coated with a thin film of the photocatalytic191 paint P using the dip-coating method (Dip-Coater RDC21-K, Bungard Elektronik GmbH

192 & Co. KG.) [57]; the photocatalytic paint supported on cellulose acetate monoliths was 193 labelled as PC. Briefly, before coating, cellulose acetate samples were soaked for 1 h with 194 distilled water and alkaline detergent (Derquim LM 01, Panreac Química, S.A.U.), 195 subsequently washed exhaustively with Milli-O water, and finally, heated up to 323 K to 196 dryness. Then, four layers of photocatalytic paint P were deposited at a withdrawal rate 197 of 0.8 mm s<sup>-1</sup> until a thin and uniform film was formed on each support surface (these 198 samples were dried at 323 K for 1 h between each layer deposition). Finally, PC samples 199 were packed into an annular photocatalytic reactor (see section 2.4) for the study of 200 *n*-decane degradation through PCO. The catalytic bed properties are also detailed in Table 201 1.

202 Scanning electron microscopy (SEM) coupled with energy dispersive X-ray (EDX) 203 analysis was performed in a FEI Quanta 400 FEG ESEM / EDAX Genesis X4M apparatus 204 equipped with a Schottky field emission gun (for optimal spatial resolution) for the 205 characterization of the surface morphology of PC500 powder, fresh PC, and used PC 206 samples (after more than 50 h of PCO experiments) as well as their chemical composition. Each sample was mounted on a double-sided adhesive tape made of carbon for its surface 207 208 observation at different magnifications; the cross-section of the fresh PC sample was also 209 measured by this technique. These SEM/EDX analyses were made at CEMUP (Centro de 210 Materiais da Universidade do Porto).

211

## 212 2.3. Experimental setup

The experimental setup is depicted in Fig. 1. A full description of the whole apparatus is given elsewhere [58]. The feed generator is composed by three mass flow controllers (MFC, El-Flow, Bronkhorst High-Tech B.V.), which allow the generation of humid air streams contaminated with *n*-decane by flowing air through distinct Woulff 217 bottles (Normax, Lda.), one containing *n*-decane and another filled with deionized water 218 (Fig. 1a). The photocatalytic system comprises (Fig. 1b): i) a solar simulator (Atlas, model 219 Suntest XLS+) with a working area of 0.110  $m^2$ , a 1.7 kW air-cooled xenon arc lamp, a 220 daylight filter and quartz filter with infrared coating; ii) a compound parabolic collector with 0.023 m<sup>2</sup> of illuminated area with electropolished anodized aluminium reflectors (to 221 222 use both direct and diffuse irradiation as well to uniform it throughout the bed); iii) 223 photoreactor composed by two concentric and axially centred tubes (the outer tube made 224 of Pyrex-glass, Duran borosilicate glass 3.3, cut-off at 280 nm, Schott-Rorhglas GmbH, 225 and the inner tube made of quartz, Quarzglas-Rohr Quarzglastechnik, GmbH & Co.); iv) an actinic lamp (Actinic BL TL 6 W, Koninklijke Philips Electronics N.V.) for catalyst 226 227 degassing and activation purposes, placed inside and axially centred in the inner tube 228 (peak at 365 nm – UVA radiation). Both inlet and outlet caps of the photoreactor have 229 four equidistant inlets to ensure a better distribution of the feed stream to the reactor. Note 230 that the tubing for inlets and outlets are made of PTFE (supplied by Vidrolab2, S.A.) that 231 minimizes the adsorption of VOCs. Table 1 also shows the tube dimensions of the 232 photoreactor; Figs. 1b1 and 1b2 schematically represent the continuous-flow photoreactor 233 from a side and frontal point of view, respectively.

n-Decane concentration histories were monitored using a gas chromatograph (MGC Fast GC, Dani Instruments S.p.A.) equipped with a flame ionisation detector (FID) and a Volcol capillary column (20 m × 0.18 mm × 1.00 µm; Supelco, Sigma-Aldrich Co. LLC.) (see Fig. 1c). The experimental setup was connected to a computer and controlled using a data acquisition board system and an in-house program developed routine written in Labview environment (NI Corporation). All connections are of 1/16" stainless steel tubing (Swagelok Company) to reduce dead volumes.

241 Additionally, by-products from the *n*-decane photooxidation were analysed at

242 steady-state, sampling the photoreactor exit stream to a Tedlar bag (232-05SKC, SKC 243 Inc.) and then transferring the sample to stainless steel tubes with Tenax TA60/80 mesh 244 (Supelco, Sigma-Aldrich Co. LLC.). After sampling, identification and quantification of 245 the reaction products was performed with a thermal desorption system (SDT 33.50, Dani Instruments S.p.A.) working in line with a GC/MSD device (a gas chromatograph GC 246 247 6890N coupled to a mass spectrometer detector MSD 5973, Agilent Technologies, Inc.). 248 The response factor of toluene (ISO 16000-6 [59]) was used to determine the 249 concentration of the major products (while for *n*-decane, specific response factor were 250 used).

#### 251 2.4. Photocatalytic experiments

252 All experiments were carried inside the chamber of the aforementioned solar 253 simulator, which can simulate a spectrum similar to that of sunlight within  $300 < \lambda < 800$ 254 nm. The incident irradiance was measured using a broadband UV radiometer (CUV 5, 255 Kipp & Zonen B.V.), placed on the outside of the outer tube and at the same height, within 256 a spectral range of 280 to 400 nm corresponding to the UV fraction of the solar irradiation. 257 At steady-state, *n*-decane photodegradation fraction ( $C_{dec, exit}$  /  $C_{dec, feed}$ , where 258  $C_{\text{dec, feed}}$  and  $C_{\text{dec, exit}}$  in ppm are the pollutant concentration on the feed and exit streams, 259 respectively) was studied for several experimental conditions: feed flow rate (75-300 260 cm<sup>3</sup> min<sup>-1</sup>, measured at 1 bar and 298 K), pollutant concentration (40-138 ppm), feed 261 relative humidity (3-40%, measured at 1 bar and 298 K), and incident irradiance (18.9-38.4 W m<sup>-2</sup>, measured for the spectral range between 280-400 nm: UV fraction of 262 263 the incident sunlight). Table 2 summarizes all the experiment conditions. Prior to all 264 experiments, the catalytic bed was degassed and the photocatalytic paint coat activated under UV radiation and by flowing 30 mL min<sup>-1</sup> (measured at 1 bar and 298 K) of 265 266 synthetic air with 40 % of relative humidity for 24 h (similar conditions as described elsewhere [41]). Before turning on the solar simulator, the catalytic bed was continuously
fed and, by means of outlet stream sampling analysis, the feed composition steadiness
was checked.

- 270 **3. Results and discussion**
- 271 *3.1. Photochemical oxidation of* n*-decane*

A blank test consisting in an experiment without photocatalyst was performed, showing no measurable *n*-decane concentration decrease (data not presented; operating conditions reported in Table 2: run 1).

275 *3.2. Photocatalytic oxidation of* n*-decane* 

276 *3.2.1.* Surface characterization of photo-TiO<sub>2</sub> powder and PC samples

277 The surface morphology of PC500 powder sample and its chemical composition 278 were determined by SEM/EDX. The SEM micrograph (Supplementary Data: Fig. A.1) 279 shows an estimated size of the photo-TiO<sub>2</sub> agglomerates of ca. 600-1500 nm. According 280 to this image, the dimension of the agglomerates range from half size up to the values 281 provided by the manufacturer (see Table 1); similar sizes are displayed in SEM pictures 282 of photocatalytic paint films loaded with the same photocatalyst and reported by Águia 283 et al. [51]. As previously mentioned by the same authors [51], EDX analysis of PC500 284 powder (Supplementary Data: Fig. A.2) indicates that both agglomerates and individual 285 particles are only made of TiO<sub>2</sub>.

The surface morphology and chemical composition of PC samples was also determined by SEM/EDX. SEM micrographs of fresh PC and used PC samples (with 50 h+ of use in PCO of *n*-decane) at three different magnifications are shown in Figs. 2a to 2d. The fresh PC images (Figs. 2a and 2c) show that the photocatalytic paint was homogeneously coated on the cellulose acetate monolith. After its use on the PCO experiments (Figs. 2b and 2d), SEM micrographs suggest that the film structure was not

292 significantly affected despite the harsh operating conditions employed. This conclusion 293 was also supported by EDX analysis of both fresh and used samples (shown in Figs. 2e 294 and 2f, respectively). According to the EDX spectra, the proportion of each element 295 remained approximately the same after the photocatalytic experiments. From SEM 296 images (Fig. 3) it was also possible to estimate the paint film thickness (ca. 5-10  $\mu$ m) and 297 the cellulose acetate monolith thickness (ca. 50 µm). Contrarily to what have been 298 observed by Lopes et al. [60] when using TiO<sub>2</sub> sol-gel films supported on cellulose acetate 299 monoliths, paint films are approximately 25-fold thicker (and more resistant) than TiO<sub>2</sub> 300 sol-gel films. These properties significantly prevent film fissures, delamination, and/or degradation. Thus, the use of paint films reveals to be an advantage in the prevention of 301 302 the catalyst/support aging.

# 303 3.2.2. Operating parameters effect on n-decane photodegradation

304 At steady-state conditions, *n*-decane photodegradation fraction ( $C_{dec, exit} / C_{dec, feed}$ ) 305 was obtained for four experimental conditions (Figs. 4-6). Fig. 4 shows the effect of the 306 feed flow rate  $(Q_{\text{feed}})$  on the *n*-decane photodegradation fraction. *n*-decane 307 photodegradation decreases as  $Q_{\text{feed}}$  increases, since a higher feed flow rate results in a 308 lower residence time, reducing the pollutant-catalyst contact period. Thereby, for a 4-fold 309 increase in  $O_{\text{feed}}$ , the photocatalytic process is 1.6, 1.9, and 2.3 times less effective, 310 respectively, for incident irradiances of 38.4, 29.1 and 18.9 W m<sup>-2</sup> (Table 2: runs 4 and 7, 311 runs 5 and 8, and runs 6 and 9, respectively). This also means that, for a higher feed flow 312 rate the incident irradiance on the catalyst surface becomes more relevant for the PCO of 313 *n*-decane: the electron-hole pairs formation is favoured by higher incident irradiances.

In Fig. 5 is shown the influence of the feed concentration on the *n*-decane photodegradation fraction. Results show a decrease in the photodegradation fraction with an increase of *n*-decane concentration. In fact, for a 3.4-fold increase in *n*-decane 317 concentration, 1.8, 2.4, and 3.6 times lower photodegradation fractions were observed for incident irradiances of 38.4, 29.1 and 18.9 W m<sup>-2</sup>, respectively (Table 2: runs 4 and 7, 318 319 runs 5 and 8, and runs 6 and 9, respectively). So, increasing the number of *n*-decane 320 molecules that enters the reactor per unit of time, a higher number of photons/hydroxyl 321 radicals are necessary to achieve the same photodegradation. Furthermore, the results 322 above suggest that the feed concentration has a more important influence on the PCO of 323 *n*-decane than the feed flow rate for the same organic load, most likely due to the 324 considerably lower surface area "usefully" available for the photocatalytic reaction. In 325 other words, despite the equivalent UV-irradiated surface area, there are more VOC 326 molecules adsorbed per surface area, restricting the generation of oxidant species from 327 adsorbed water and oxygen (namely, hydroxyl radicals, peroxide radicals, and superoxide 328 radicals).

Although there are plenty of studies describing the influence of feed relative 329 330 humidity on the photodegradation of alkanes, conclusions are still not clear [10, 61]. 331 Twesme et al. [62] and Zhang and Liu [63] pointed out 40% and 20% of relative humidity, 332 respectively, as the optimum conditions regarding water content to obtain the highest 333 degradation rates in their studies. Shang et al. [64] demonstrated in their studies that the 334 degradation rate of *n*-heptane decreases as the relative humidity was increased from 0 to 335 60%. In fact, the presence of vapour water molecules has two opposing effects: i) inhibits 336 the degradation by competitive adsorption to the photocatalyst surface (for feed streams 337 with high water vapour content) [6, 65]; ii) accelerates the degradation by promoting 338 hydroxyl radicals formation [25]. Fig. 6 shows a slight relative increase (3%) of the *n*-decane photodegradation for the highest irradiance value (38.4 W m<sup>-2</sup>) and within the 339 340 relative humidity range of 3 % to 40 %. On the other hand, it was found that for the lower 341 irradiance values, particularly for 18.9 W m<sup>-2</sup>, its effect on the *n*-decane photodegradation becomes more relevant: for the same relative humidity increment, the *n*-decane photodegradation is 3% (from run 16 to run 1) to 25% (from run 18 to run 3) more efficient with a 2-fold reduction of the incident irradiation (from 38.4 to 18.9 W m<sup>-2</sup>). This supports the important role of hydroxyl radicals in photocatalytic processes due to the lower amount of surface electron-hole pairs available on the catalyst surface to react with the pollutant molecules.

It should be pointed out that after 50 h under simulated solar irradiation and continuous feed (humid air contaminated with *n*-decane), similar photodegradations were obtained under the same operating conditions (data not shown). Considering the up-stated for SEM analysis (see section 3.2.1), it is suggested that PC deterioration was negligible.

352 3.2.3. Simulation and predictive studies of n-decane kinetics through PCO

353 Several models have been proposed in the literature for simulating VOC 354 photocatalytic oxidation kinetics [58, 60]. Table 3 describes the complete mathematical 355 model combined with three different Langmuir-Hinshelwood reactions rate expressions. 356 The numerical solution of the mathematical model was performed in gPROMS 357 environment (Process System Enterprise, London, UK) using the orthogonal collocation 358 on finite elements method. The number of elements used was 90 with two interior 359 collocation points (third order polynomials) in each element of the photocatalytic bed. 360 The simulations were performed with an absolute and relative tolerance of  $1 \times 10^{-5}$ . First, 361 parameters were estimated using a sequential quadratic programming algorithm [60]; 362 then, the mathematical model was employed for simulating the PCO of *n*-decane. Table 363 3 reports the estimated kinetic and adsorption equilibrium parameters.

Results shows that the mathematical model with the Langmuir-Hinshelwood kinetic reaction rate expression RE-3 (bimolecular competitive two types of sites rate expression) generally produced better fitting results within the operational conditions 367 studied than models RE-1 or RE-2 (bimolecular competitive one type of sites or 368 bimolecular non-competitive two types of sites rate expressions) (Figs. 4-6). This means 369 that both *n*-decane and water molecules must be considered independent and targeting 370 different active sites of the catalyst surface. The surface active sites competition between 371 the two types of molecules cannot be disregarded because, despite the higher number of 372 parameters required by RE-3, this rate expression is more suitable to describe the 373 experimental data (see the statistical analysis reported in Table 3). Contrarily to the 374 previous reported models of PCO [58, 60], it was necessary to include an incident 375 irradiance exponential order constant (n). The radial effect of the UV irradiation passing 376 through the PC samples and its consequent reflection and refraction were not considered; 377 moreover, the mathematical model neglects any partial UV absorption by the PC samples. 378 Nevertheless, the UV irradiance on PCO of *n*-decane could be fitted by an irradiance 379 exponential order constant n = 0.8, as can be seen throughout the paper (Figs. 4-6).

The closest results to our data regarding gas-phase PCO of *n*-decane were obtained by Debono *et al.* [66]. However, these authors performed UVA-photocatalytic experiments of *n*-decane over  $TiO_2$  powder dispersed at the bottom of a batch reactor, and employing *n*-decane-polluted air stream at ppb level. Therefore and only for these conditions Debono *et al.* [66] were able to provide a photocatalytic lab-scale setup effective for complete *n*-decane photodegradation.

Considering that the mathematical model described successfully the reported experiments, simulations can now be performed to obtain insights concerning the effect of each operating variable on the process performance. The effect of the lab-unit geometrical parameters on the PCO of *n*-decane was assessed (*e.g.*, photoreactor length  $L_{\rm R}$ ) within the operating condition studied, aiming unit geometric optimization and rescaling. Fig. 7 shows the *n*-decane photodegradation fraction profiles, considering

392 photoreactors of different lengths  $(L_R)$ . It can be seen that, when the operating conditions 393 of run 3 are employed (lowest incident irradiance, and intermediate feed flow rate and 394 *n*-decane concentration), a 1.5-fold increase of the photoreactor length yields to a 395 n-decane photodegradation enhancement of 85% (see Fig. 7a). Moreover, for a 396 photoreactor  $2 \times \text{longer}$ , complete *n*-decane photodegradation is attained (Fig. 7a). On the 397 other hand, Fig. 7b predicts how *n*-decane photodegradation fraction is affected as a 398 function of the photoreactor length when the highest incident irradiance and feed flow 399 rate are employed (run 7). For a 1.5 times longer photoreactor than the experimentally 400 employed, a 76% *n*-decane photodegradation enhancement is observed. If the reactor is 401 twice the length ( $L_R = 0.32$  m), only 1% of *n*-decane feed is predictively unreacted; 402 complete *n*-decane photodegradation is attained when using a  $\sim 3$  times longer 403 photoreactor.

#### 404 *3.3. Reaction mechanism for the PCO of n-decane*

405 The degradation mechanisms of alkanes and the corresponding formation of its 406 by-products have been studied recently [61, 64, 66-69]. According to the previously cited 407 authors it was found that ketones and aldehydes are the main intermediates of *n*-decane 408 photochemical reaction. Minabe et al. [70] reported that gas-phase photooxidation of long 409 organic chains over TiO<sub>2</sub> thin-films only produces CO<sub>2</sub> and H<sub>2</sub>O. It was suggested that 410 both reactants and intermediates were continuously adsorbed on the TiO<sub>2</sub> surface. Within 411 this work, identification and quantification of the *n*-decane photocatalytic reaction by-412 products were monitored by GC/MSD (Supplementary Data: Table A.1), for the 413 experimental conditions of run 1 (previously described in Table 2). The identified by-414 products (and their concentration) were: unreacted *n*-decane (4.32 ppm), *n*-hexane (0.035 415 ppm), *n*-heptane (0.028 ppm), *n*-octane (0.007 ppm), *n*-nonane (0.036 ppm), *n*-undecane 416 (0.005 ppm), 4-methylnonane (0.006 ppm), 2,6-dimethyloctane (0.009 ppm), butanoic

417 acid (0.022 ppm), propanoic acid (0.072 ppm), and butanal (0.016 ppm). Therefore and 418 based on the nature of the identified compounds, a reaction mechanism under wet air 419 (40%) is proposed and schematized in scheme 1. According to scheme 1, n-decane 420 undergoes a cleavage into radicals - cracking - by a hydroxyl radical. Taking into 421 consideration that alkyl radical stability increases along the series from methyl to primary, 422 followed by secondary, and then by tertiary carbon, the energy required to create them 423 decreases [71]. So, in the case of straight-chain alkanes, secondary carbons are oxidized 424 by hydroxyl radical rather than primary ones. Nonetheless, from scheme 1 and supported 425 by literature [64, 71-73], it is assumed the formation of both primary and secondary alkyl 426 radicals. After homolytic cleavage of *n*-decane four paths can take place: 1) radical 427 recombination generating new alkane hydrocarbons such as *n*-hexane, *n*-octane, or 2,6-428 dimethyloctane (Table 3); 2) hydrogen abstraction reactions leading to the formation of 429 alkanes and alkenes; 3) reaction with adsorbed O<sub>2</sub> producing a highly reactive superoxide 430 radicals; 4) oxidation by hydroxyl radicals forming alcohols.

431 Several authors [24, 64, 67, 73] reported the rapidly dehydration of alcohols into 432 alkenes or oxidation into corresponding ketones or aldehydes (see scheme 1, path 4); 433 alkenes could be degraded into aldehydes as reported by Djeghri and Teichner [72] 434 whereas aldehydes could suffer double oxidation by hydroxyl radicals into carboxylic 435 acid [24, 74, 75] as it was detected the presence of propanoic and butanoic acid. An 436 alternative approach was suggested by Kominami et al. [76] after observing the formation 437 of an ester from the recombination of the aldehyde and its intermediate. Then, according 438 to Augugliaro *et al.* and Peral *et al.* [24, 25], ester could be adsorbed on the TiO<sub>2</sub> surface 439 where it would be dissociated into alkoxy and carboxylate radical. The alkoxy form an 440 aldehyde and the carboxylate radical could produce alkyl radicals and carbon dioxide 441 leading to alkanes after radical recombination or alkenes after hydrogen abstraction

442 reaction. Carboxylate radical could also be formed by oxidation by hydroxyl radical of 443 carboxylic acid which would lead to the formation of alkyl radicals and CO<sub>2</sub> in a process 444 called decarboxylative dimerization. On the other hand, several authors [77-79] have proposed the reaction between ketones and adsorbed O2, forming an unstable ketone 445 446 diolate complex onto the  $TiO_2$  surface. Consequently, the diolate complex would rapidly 447 be dissociated into carboxylate which would lead to the formation of alkyl radicals and 448 carbon dioxide. These radicals would be rapidly oxidized into alcohols and, then, 449 aldehydes [80]. This approach may explain the absence of ketones and presence of 450 butanal.

451 Considering that  $C_{i, C-dec}$  refers to the carbon atoms concentration of compound *i* 452 formed by *n*-decane photodegradation (all unreacted *n*-decane and its by-products 453 produced), it can be defined as:

454 
$$C_{i,C-dec} = \frac{C_i}{M_i} \cdot n(C) \cdot M(C)$$
 (eq. 8)

455 where  $C_i$  [ppm] and  $M_i$  [g mol<sup>-1</sup>] are the gas phase concentration and molecular weight of 456 compound i, respectively, n(C) is the number of carbon atoms of each component *i* 457 molecule, and M(C) [g mol<sup>-1</sup>] is the molecular weight of a carbon atom. Thus, the 458 mineralization efficiency ( $\eta_{\min}$  in %) can be determined through eq. 9.

459 
$$\eta_{\min}[\%] = \left[1 - \frac{\sum_{i} (C_{i, C-dec})_{exit}}{\sum_{i} (C_{i, C-dec})_{feed}}\right]$$
(eq. 9)

Thus, considering the carbon atoms concentration of each identified and quantified byproduct resulting from the *n*-decane molecules photodegradation (experimental conditions reported in Table 1: run 1) more than 99% of the *n*-decane degraded (~94% of *n*-decane fed) was completely mineralized into CO<sub>2</sub> and H<sub>2</sub>O. This result is in agreement to what Debono *et al.* [66] disclosed in their previous work: the total carbon atoms concentration of all by-products formed by *n*-decane photodegradation is lower than 5%.

#### 466 **4.** Conclusion

467 The use of an annular lab-photoreactor under simulated solar irradiation has 468 shown to be inefficient for the photochemical reaction of gaseous *n*-decane and extremely 469 effective on the photocatalytic process over a photo-TiO<sub>2</sub> paint. Under simulated solar 470 irradiation, the gas-phase photocatalytic experiments showed that highest *n*-decane 471 photodegradation (98%) was attained at the lowest  $Q_{\text{feed}}$  (75 cm<sup>3</sup> min<sup>-1</sup>) and  $C_{\text{dec, feed}}$ (41 ppm), and highest  $RH_{\text{feed}}$  (40%) and I (38.4 W m<sup>-2</sup>). Feeding the photoreactor with 472 473 the double flow rate, the *n*-decane photodegradation decreases from 96 to 62% (run 1 and 474 7). Alternatively, when the *n*-decane concentration on the feed stream is doubled, the 475 remaining unreacted *n*-decane fed drops from 4 to 46% (run 1 and 13). It was also 476 observed that the water vapour content effect on the PCO of *n*-decane is more pronounced 477 under lower irradiances, i.e., from ~71 to 56% (run 3 and 18).

A phenomenological model, assuming a Langmuir-Hinshelwood mechanism (bimolecular competitive with two types of sites) was able to describe the *n*-decane photodegradation. It was observed proposed that both species compete for adsorption within different specific active sites (type 1 and 2) of the catalyst surface. Considering the type of by-products identified, a reaction mechanism for *n*-decane photodegradation under the conditions used was proposed.

For all reasons stated before and considering the well-known wide range of paint applications, the results reported seem quite promising for the treatment of indoor and outdoor air. Further research should focus in studying the role of interfering pollutants, as NO<sub>2</sub>, and also the eventual production of acetaldehyde and formaldehyde as subproducts.

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500

501 Appendix A. Supplementary Data

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# **Table captions**

**Table 1.** Catalyst and paint properties; catalytic bed characteristics; photoreactor

dimensions employed in the gas-phase PCO of *n*-decane under simulated solar irradiation.

- **Table 2.** Experimental conditions employed in the study of *n*-decane photodegradation.
- **Table 3.** Mathematical model, boundary conditions, kinetic reaction rate expressions
- 655 used for estimation of the kinetic and adsorption equilibrium parameters of the PCO of
- *n*-decane; Estimated kinetic and adsorption equilibrium parameters of the mathematical
- model.

#### 659 **Figure Captions**

Fig. 1. Schematic representation of the experimental set-up and the continuous-flow 661 photoreactor: a) lab-scale unit used for the generation of air streams containing *n*-decane 662 and water vapour; b) sunlight simulator containing the photoreactor:  $b_1$ ) from a side point 663 of view and b<sub>2</sub>) from a frontal point of view; c) master gas chromatograph analytic system 664 used for the analysis of the photoreactor feed and exit streams. Reprinted (adapted) with 665 permission from Lopes et al. [58]. Copyright © 2012, Elsevier. 666 Fig. 2. SEM micrographs (a-d) and EDX spectra (e, f) of PC before (left-side images) and

- 667 after 50 h+ of use (right-side images) in PCO of *n*-decane.
- 668 Fig. 3. Photographs (a-b) and SEM micrographs (c-d) of PC after 50 h+ of use in PCO of 669 *n*-decane.
- Fig. 4. Influence of feed flow rate ( $Q_{\text{feed}}$ ) on *n*-decane photodegradation fraction 670 671  $(C_{\text{dec, exit}}/C_{\text{dec, feed}}, \text{ at steady-state conditions})$ : experimental points for incident irradiances measured within 280-400 nm (sunlight UV fraction) of 38.4 W·m<sup>-2</sup> (�), 29.1 672  $W \cdot m^{-2}$  (**D**), and 18.9  $W \cdot m^{-2}$  (**A**), and RE-1 (---), RE-2 (---), and RE-3 (---); 673 674  $C_{\text{dec, feed}} = 73 \text{ ppm}, RH_{\text{feed}^a} = 40\%$ , and T = 298 K; operation conditions reported in Table 1; \* measured at 298 K and 1 bar. 675
- 676 Fig. 5. Influence of the inlet concentration ( $C_{dec, feed}$ ) on *n*-decane photodegradation 677 fraction ( $C_{dec, exit} / C_{dec, feed}$ , at steady-state conditions): experimental points for incident irradiances measured within 280-400 nm (sunlight UV fraction) of 38.4 W·m<sup>-2</sup> (�), 29.1 678  $W \cdot m^{-2}$  (**D**), and 18.9  $W \cdot m^{-2}$  (**A**), and RE-1 (---), RE-2 (---), and RE-3 (---); 679  $Q_{\text{feed}}^* = 150 \text{ cm}^3 \cdot \text{min}^{-1}$ ,  $RH_{\text{feed}}^a = 40\%$ , and T = 298 K; operation conditions reported in 680 Table 2; \* measured at 298 K and 1 bar. 681 682 Fig. 6. Influence of the feed relative humidity  $(RH_{feed})$  on *n*-decane photodegradation
- 683 fraction ( $C_{dec, exit} / C_{dec, feed}$ , at steady-state conditions): experimental points for incident

irradiances measured within 280-400 nm (sunlight UV fraction) of 38.4 ( $\diamondsuit$ ), 29.1 ( $\square$ ), and 18.9 W·m<sup>-2</sup> ( $\blacktriangle$ ), and RE-1 (---), RE-2 (---), and RE-3 (---);  $Q_{\text{feed}}^* = 150 \text{ cm}^3 \cdot \text{min}^{-1}$ ,  $C_{\text{dec, feed}} = 73 \text{ ppm}$ , and T = 298 K; operation conditions reported in Table 2; \* measured at 298 K and 1 bar.

688 Fig. 7. *n*-Decane photodegradation fraction profiles ( $C_{dec, exit}/C_{dec, feed}$ , at steady-state

689 conditions) for photoreactors with different lengths  $[L_R]$ : 0.16 (—), 0.24 (– –), 0.32 (– –

- 690 -), and 0.48 m (· · ·); (a)  $C_{\text{dec, feed}} = 73 \text{ ppm}$ ,  $Q_{\text{feed}}^* = 150 \text{ mL min}^{-1}$ , and  $I = 18.9 \text{ W m}^{-2}$
- 691 (measured within 280-400 nm: sunlight UV fraction); (b)  $C_{dec, feed} = 73 \text{ ppm}$ ,
- 692  $Q_{\text{feed}}^* = 300 \text{ mL min}^{-1}$ , and  $I = 38.4 \text{ W m}^{-2}$  (measured within 280–400 nm: sunlight UV
- 693 fraction);  $RH_{\text{feed}}^* = 30\%$ , and T = 298 K; operation conditions reported in Table 2 (runs 3
- and 7, respectively) (\* measured at 298 K and 1 bar); experimental data (points);
- 695 mathematical modelling with RE-3 (lines).

# 696 Scheme Captions

- 697 **Scheme 1.** Schematic representation of the reaction pathways proposed for the gas-phase
- 698 degradation of *n*-decane under simulated solar irradiation (R: alkyl roots or hydrogen).

# Table 1

Catalyst and paint properties; catalytic bed characteristics; photoreactor dimensions employed in the gas-phase PCO of *n*-decane under simulated solar irradiation.

Catalyst and Paint [51, 52]						
	Manufacturer	PC500 (Millennium)				
	Crystal structure	>99% Anatase				
	Crystal size [nm]	5-10				
PC500	Shape	Agglomerates				
	Surface area $[m^2 g^{-1}]$	345				
	Agglomerate size [µm]	1.2-1.7				
	Shape	Agglomerates				
	Pigmentary TiO <sub>2</sub>	18 wt.% (wet basis)				
	Water	30 wt.% (wet basis)				
Exterior water-based	Extenders (CaCO <sub>3</sub> and silicates)	18 wt.% (wet basis)				
vinyl paint	Polymer extender slurry	8 wt.% (wet basis)				
	Binder slurry	20 wt.% (wet basis)				
	Additives (in slurry)	6 wt.% (wet basis)				
Catalytic bed (PC)						
	$TiO_2$ content (wet basis)					
	Pigmentary	9 wt.% (wet basis)				
Catalyst (P)	PC500	9 wt.% (wet basis)				
Catalyst (r)	Thin-film properties					
	$m_{\rm P} [g]$	1.052				
	$\rho_{\rm P} [{ m g \ cm^{-3}}]$	2.61				
	<i>m</i> <sub>C</sub> [g]	2.006				
Support (C)	$\rho_{\rm C} [{\rm g}{\rm cm}^{-3}]$	1.30				
	$d_{\rm ch}$ [cm]	0.9				
Porosity	Э	0.991				
Photoreactor						
Outer tube	$d_{\rm ot,e}$ [cm]	5.00				
(Pyrex-glass)	$d_{\rm ot,i} [{\rm cm}]$	4.64				
Inner tube	$d_{\rm in,e} [{\rm cm}]$	2.00				
(quartz)	$d_{\text{in,i}}$ [cm]	1.64				
Photoreactor	$L_{\rm R}$ [cm]	16.0				
1 110101000101	$V_{\rm R} [{\rm cm}^3]$	220				

photodegradation.						
Dun	$Q_{\mathrm{feed}}^{*}$	$C_{ m dec, feed}$	$RH_{\text{feed}}^{*}$	$I^{\#}$		
Run	$[\mathrm{cm}^3 \mathrm{min}^{-1}]$	[ppm]	[%]	$[W m^{-2}]$		
1 <sup>a)</sup>	150	73	40	38.4		
2	150	73	40	29.1		
2 3	150	73	40	18.9		
4	75	73	40	38.4		
5	75	73	40	29.1		
6	75	73	40	18.9		
7	300	73	40	38.4		
8	300	73	40	29.1		
9	300	73	40	18.9		
10	150	40	40	38.4		
11	150	40	40	29.1		
12	150	40	40	18.9		
13	150	138	40	38.4		
14	150	138	40	29.1		
15	150	138	40	18.9		
16	150	73	3	38.4		
17	150	73	3	29.1		
18	150	73	3	18.9		
* • •						

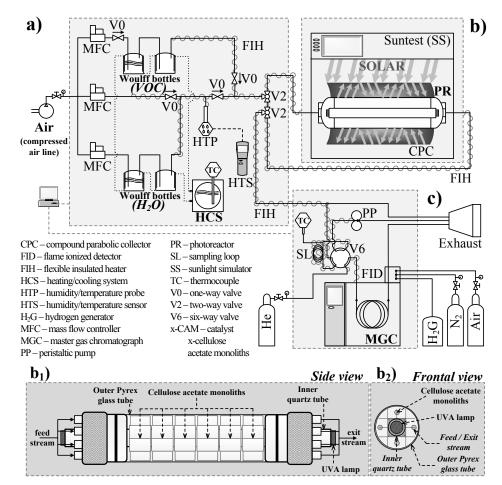
Table 2 Experimental conditions employed in the study of *n*-decane photodegradation.

\* Measured at 298 K and 1 bar.
# Measured within 280–400 nm (sunlight UV fraction).
a) Operating conditions used for photochemical experiment.

# Table 3

Mathematical model, boundary conditions, kinetic reaction rate expressions used for estimation of the kinetic and adsorption equilibrium parameters of the PCO of *n*-decane; Estimated kinetic and adsorption equilibrium parameters resulting of the mathematical model.

Mathematical	model. correlations. paran	neters, and bou	ndary condit	ions [58, 60]				
Mathematical model, correlations, parameters, and boundary conditions [58, 60]Material balance for each component $i$ $\frac{d}{dz} \left( \varepsilon D_{ax} \frac{dC_i}{dz} \right) - \frac{d}{dz} \left( \overline{u}_{0,ch} C_i \right) - v_i r = 0$								
Axial dispersion	n (laminar flow) [81-84]	$D_{\rm ax} = D_{\rm m} + (1)$	$(192)[(\overline{u}_{0,ch}^2 d_{ch}^2)]$	$/(\varepsilon D_m)$ ]				
Molecular diffusivity of the mixture $D_{\rm m} \cong \frac{1}{N} \sum_{i=1}^{N} D_{{\rm m},i}$ , with $D_{{\rm m},i} = (1 - y_i) \sum_{\substack{i=1 \ j \neq i}}^{n} \frac{D_{{\rm i}j}}{y_i}$								
Binary diffusion	n coefficient [85-88]	$D_{ij} = \frac{1.41 \times 10}{p}$	$=\frac{1.41\times10^{-7}T^{1.75}\left[\frac{1}{2}\left(M_{i}^{-1}+M_{j}^{-1}\right)\right]^{1/2}}{p\left[\left(\Sigma_{v}\right)_{i}^{1/3}+\left(\Sigma_{v}\right)_{j}^{1/3}\right]^{2}}$					
	Superficial velocity (in the cross-section of each channel) $\overline{u}_{0,ch} = Q_{\text{feed}} \left[ \pi \left( \frac{1}{2} d_{\text{ot,i}} \right)^2 - \pi \left( \frac{1}{2} d_{\text{in,e}} \right)^2 \right]^{-1}$							
Component i	N <sub>2</sub> O <sub>2</sub>	Н	2O	dec				
$M_{\rm i} [\rm g \cdot \rm mol^{-1}]$	28.01 32.00	18	3.02	142.28				
$(\Sigma_v)_i$	18.5 16.3	13		209.8				
× /1	Photoreactor feed ( $z = 0$ ) Photoreactor exit ( $z = L_R$ )							
Boundary		101	10	l í				
conditions	$u_{0,\text{feed}} C_{i,\text{feed}} = \overline{u}_{0,\text{ch}} C_{i}$	$-\varepsilon D_{ax} \frac{uC_i}{L}$	$\frac{aC_i}{L}$	= 0				
		$dz \mid_{z=0}$	dz	$ _{z=L_{R}}$				
Kinetic reaction	on rate expressions [3, 6, 58	, 60, 89-95]						
RE-1 $r_{dec} = I^{n} \cdot k \left( \frac{K_{dec} K_{H_{2}O} C_{dec} C_{H_{2}O}}{\left( 1 + K_{dec} K_{H_{2}O} C_{dec} C_{H_{2}O} \right)^{2}} \right)$ Langmuir-Hinshelwood bimolecular competitive one type of sites								
RE-2 $r_{dec} = I^n \cdot k \left( \frac{K_{dec} C_{dec}}{1 + K_{dec} C_{dec}} \right) \left( \frac{K_{H_2O} C_{H_2O}}{1 + K_{H_2O} C_{H_2O}} \right)$								
RE-3 $Iangmuir-Hinshelwood bimolecular non-competitive two types of sites$ $r_{dec} = I^{n} \cdot k \left( \frac{K_{dec}C_{dec}}{1 + K_{dec}C_{dec} + K_{H_{2}O}C_{H_{2}O}} \right) \left( \frac{K'_{H_{2}O}C_{H_{2}O}}{1 + K'_{dec}C_{dec} + K'_{H_{2}O}C_{H_{2}O}} \right)$ $Langmuir-Hinshelwood bimolecular competitive two types of sites$								
Estimated nor	0	cular competitive i	wo types of sites					
Estimated para	n rate expressions	RE-1	RE-2	RE-3				
KINCLIC TEACTION	1	0.8	0.8	0.8				
Vinatio 1	$n = k \text{ [mol m}^{-2} \text{ s}^{-1} (\text{W}^{-1} \text{ m}^{2})^{n} \text{]}$	$0.8 \\ 1.0 \times 10^{-5}$	0.8 $3.2 \times 10^{-6}$	$0.8 \\ 2.8 \times 10^{-6}$				
Kinetic and	$K_{\text{dec}} [\text{M}^{-1}]$	1.0 × 10 *	$3.2 \times 10^{-1}$	2.8 × 10 4498				
adsorption	$K_{\text{dec}}$ [M <sup>-1</sup> ]	$9.7 \times 10^{-5}$	$1.5 \times 10^{-4}$	$1.0 \times 10^{-8}$				
equilibrium	-	9.7 ~ 10	1.3 × 10					
parameters	$K'_{\rm dec} [M^{-1}]$			905 4 C × 10 <sup>-4</sup>				
	$K_{\rm H_{2}O} [\rm M^{-1}]$	0.764		$4.6 \times 10^{-4}$				
Statistics	$R^2$	0.764	0.912	0.954				
	$S^{2}_{R} \times 10^{7} \text{ [mol}^{2} \text{ m}^{-4} \text{ s}^{-2} \text{]}$	3.84	1.43	0.874				



703

**Fig. 1.** Schematic representation of the experimental set-up and the continuous-flow photoreactor: a) lab-scale unit used for the generation of air streams containing *n*-decane and water vapour; b) sunlight simulator containing the photoreactor:  $b_1$ ) from a side point of view and  $b_2$ ) from a frontal point of view; c) master gas chromatograph analytic system used for the analysis of the photoreactor feed and exit streams. Reprinted (adapted) with permission from Lopes *et al.* [58]. Copyright © 2012, Elsevier.

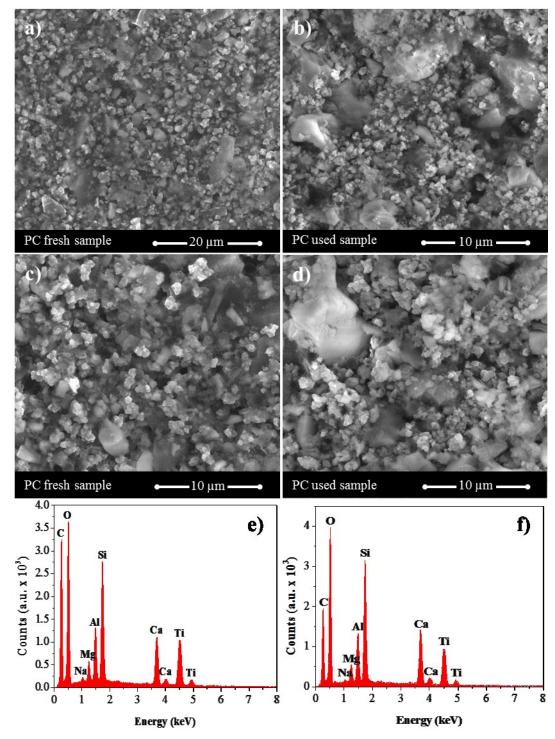
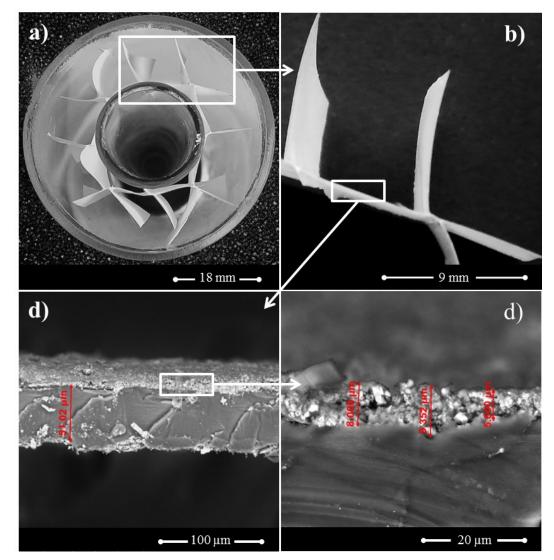


Fig. 2. SEM micrographs (a-d) and EDX spectra (e, f) of PC before (left-side images) and
after 50 h+ of use (right-side images) in PCO of *n*-decane.



- **Fig. 3.** Photographs (a-b) and SEM micrographs (c-d) of PC used in PCO of *n*-decane.

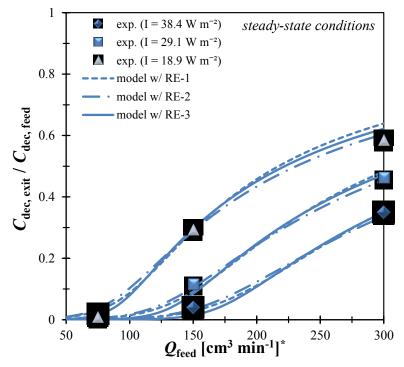




Fig. 4. Influence of feed flow rate ( $Q_{\text{feed}}$ ) on *n*-decane photodegradation fraction ( $C_{\text{dec, exit}} / C_{\text{dec, feed}}$ , at steady-state conditions): experimental points for incident irradiance measured within 280-400 nm (sunlight UV fraction) of 38.4 W·m<sup>-2</sup> ( $\diamondsuit$ ), 29.1 W·m<sup>-2</sup> ( $\square$ ), and 18.9 W·m<sup>-2</sup> ( $\bigtriangleup$ ), and RE-1 (- - -), RE-2 (- · -), and RE-3 (----);  $C_{\text{dec, feed}} = 73$  ppm, *RH*<sub>feed</sub><sup>a</sup> = 40%, and *T* = 298 K; operation conditions reported in Table 1; \* measured at 298 K and 1 bar.

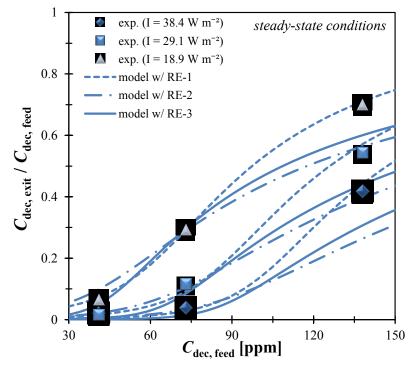




Fig. 5. Influence of the inlet concentration ( $C_{dec, feed}$ ) on *n*-decane photodegradation fraction ( $C_{dec, exit} / C_{dec, feed}$ , at steady-state conditions): experimental points for incident irradiance measured within 280-400 nm (sunlight UV fraction) of 38.4 W·m<sup>-2</sup> ( $\blacklozenge$ ), 29.1 W·m<sup>-2</sup> ( $\blacksquare$ ), and 18.9 W·m<sup>-2</sup> ( $\blacktriangle$ ), and RE-1 (- - -), RE-2 (- · -), and RE-3 (---);  $Q_{feed}^* = 150 \text{ cm}^3 \cdot \text{min}^{-1}$ ,  $RH_{feed}^a = 40\%$ , and T = 298 K; operation conditions reported in Table 2; \* measured at 298 K and 1 bar.

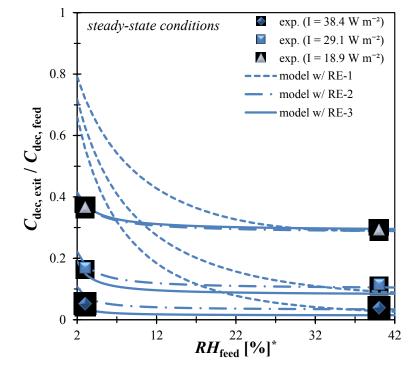




Fig. 6. Influence of the feed relative humidity ( $RH_{\text{feed}}$ ) on *n*-decane photodegradation fraction ( $C_{\text{dec, exit}} / C_{\text{dec, feed}}$ , at steady-state conditions): experimental points for incident irradiance measured within 280-400 nm (sunlight UV fraction) of 38.4 W·m<sup>-2</sup> ( $\diamondsuit$ ), 29.1 W·m<sup>-2</sup> ( $\square$ ), and 18.9 W·m<sup>-2</sup> ( $\blacktriangle$ ), and RE-1 (- - -), RE-2 (- · -), and RE-3 (---);  $Q_{\text{feed}}^* = 150 \text{ cm}^3 \cdot \text{min}^{-1}$ ,  $C_{\text{dec, feed}} = 73 \text{ ppm}$ , and T = 298 K; operation conditions reported in Table 2; \* measured at 298 K and 1 bar.

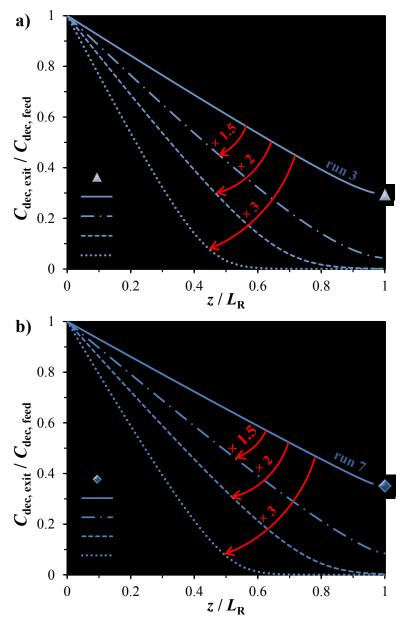
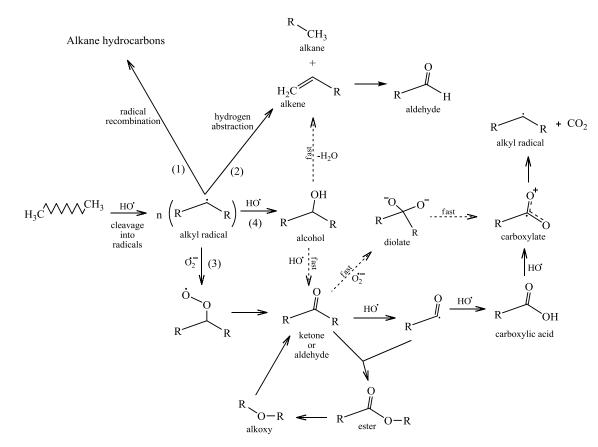




Fig. 7. *n*-Decane photodegradation fraction profiles ( $C_{dec, exit}/C_{dec, feed}$ , at steady-state 746 conditions) for photoreactors with different lengths [ $L_R$ ]: 0.16 (—), 0.24 (– –), 0.32 (– – 747 -), and 0.48 m ( $\cdot \cdot \cdot$ ); (a)  $C_{\text{dec, feed}} = 73 \text{ ppm}$ ,  $Q_{\text{feed}}^* = 150 \text{ mL min}^{-1}$ , and  $I = 18.9 \text{ W m}^{-2}$ 748 (measured within 280-400 nm: sunlight UV fraction); (b)  $C_{dec, feed} = 73 \text{ ppm}$ , 749  $Q_{\text{feed}}^* = 300 \text{ mL min}^{-1}$ , and  $I = 38.4 \text{ W m}^{-2}$  (measured within 280–400 nm: sunlight UV 750 fraction);  $RH_{\text{feed}}^* = 30\%$ , and T = 298 K; operation conditions reported in Table 2 (runs 3 751 and 7, respectively) (\* measured at 298 K and 1 bar); experimental data (points); 752 753 mathematical modelling with RE-3 (lines).



**Scheme 1.** Schematic representation of the reaction pathways proposed for the gas-phase

